

Corrections to the Linvill Normalization Procedure
in the NEC Basic Scattering Code

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An error has been found in the Linvill coupling section of the NEC-Basic Scattering Code Version 2.2 (NEC-BSC2.2) [Marhefka, 1982] subroutine OUTPUT. Figure 1 lists the coupling section of subroutine OUTPUT before the error was corrected. On lines 339 and 340 of Figure 1, the short-circuit driving point admittances are incorrectly calculated as the inverse of the open-circuit driving point impedances, i.e., $y_{11} = 1/z_{11}$ and $y_{22} = 1/z_{22}$. The correct expressions for the short-circuit driving point admittances are given in Equation 1.

$$y_{11} = \frac{z_{22}}{z_{11} z_{22} - z_{12} z_{21}} \quad (1a)$$

$$y_{22} = \frac{z_{11}}{z_{11} z_{22} - z_{12} z_{21}} \quad (1b)$$

However, the conversion from a z-parameter to a y-parameter representation was unnecessary. An important property of consistent two-port systems is that relationships between variables and parameters in any two-port representation will have the same form as the relationships between the corresponding variables, parameters, and terminations of any other two-port representation [Linvill, 1961]. In other words, power ratios will have the same form regardless of whether one uses the z,y,h or g-parameter representations for the two-port model. Therefore, since the Basic

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323      C!!!  ANTENNA TO ANTENNA COUPLING REPRESENTATION
324      WRITE(6,300)
325      WRITE(6,100)
326      WRITE(6,100)
327      WRITE(6,821)
328      821  FORMAT(' ANTENNA COUPLING VIA THE REACTION PRINCIPLE'///)
329      WRITE(6,150)
330      IF(LRECT.AND..NOT.LFQG) WRITE(6,823)
331      823  FORMAT(1H ,6X,'X',9X,'Y',9X,'Z',9X,'MAGNITUDE',5X,'PHASE',6X
332      2,'MAG.**2',8X,'DB')
333      IF(.NOT.LRECT.AND..NOT.LFQG) WRITE(6,824)
334      FORMAT(1H ,6X,'R',7X,'THETA',6X,'PHI',8X,'MAGNITUDE',5X
335      2,'PHASE',6X,'MAG.**2',8X,'DB')
336      IF(LFQG) WRITE(6,825)
337      825  FORMAT(1H ,15X,'FREQ.',16X,'MAGNITUDE',5X,'PHASE',6X
338      2,'MAG.**2',8X,'DB')
339      IF(IPRAD.EQ.4) YR11=REAL(1./Z11)
340      IF(IPRAD.EQ.4) YR22=REAL(1./Z22)
341      IMAX=10*NSN+1
342      DO 820 I=NBN,NEN,NSN
343      IM=I-1
344      CTM=0.5*BABS(CT(I))
345      CTP=DPR*BTAN2(AIMAG(CT(I)),REAL(CT(I)))
346      GO TO (815,830,835,840),IPRAD
347      C!!!  UNNORMALIZED REACTION REPRESENTATION
348      815  CTM2=CTM*CTM
349      CTDB=10.*BLOG10(CTM2)
350      GO TO 850
351      C!!!  IMPEDANCE REPRESENTATION
352      830  Z12=CT(I)/(CI11*CI22)
353      CTM2=BABS(Z12)
354      CTDB=DPR*BTAN2(AIMAG(Z12),REAL(Z12))
355      GO TO 850
356      C!!!  MODIFIED FRII'S REPRESENTATION
357      835  CTM2=0.25*CTM*CTM/(PRAD*PRADR)
358      CTDB=10.*BLOG10(CTM2)
359      GO TO 850

360      C!!!  LINVILLE REPRESENTATION
361      840  Z12=CT(I)/(CI11*CI22)
362      Y12=Z12/(Z11*Z22-Z12*Z12)
363      YY12=Y12*Y12
364      YL=BABS(YY12)/(2.*YR11*YR22-REAL(YY12))
365      YYL=YL*YL
366      CTM2=0.5*YL*(1.+0.25*YYL)
367      IF(YL.LT.0.01) GO TO 845
368      YYLS=1.-YYL
369      CTM2=(1.-SQRT(YYLS))/YL
370      845  CTDB=10.*BLOG10(CTM2)
371      850  CONTINUE
372      IF(LFQG) GO TO 818
373      RXP=RXS+RXI*IM
374      TYP=TYS+TYI*IM
375      PZP=PZS+PZI*IM
376      WRITE(6,810) RXP,TYP,PZP,CTM,CTP,CTM2,CTDB
377      GO TO 819
378      818  FQG=FQGS+FQGI*IM
379      WRITE(6,811) FQG,CTM,CTP,CTM2,CTDB
380      819  IF(I.GT.IMAX) IMAX=IMAX+10*NSN
381      IF(I.EQ.IMAX) WRITE(6,400)
382      820  CONTINUE
383      IF(I.NE.IMAX) WRITE(6,400)
384      WRITE(6,100)
385      WRITE(6,100)
386      RETURN
387      END

```

Figure 1. The original listing of the antenna coupling section of subroutine NEC-BSC2.2 OUTPUT.

Scattering Code naturally calculates the open-circuit parameters (z-parameters), it will be more convenient to use these parameters to determine the variables associated with the Linvill coupling method.

In addition to the above calculation error, a labeling error exists. On line 354 of Figure 1 the phase angle of the mutual impedance is calculated. However, in the line-printer output, this phase angle is incorrectly labeled as a dB value as indicated by Format statements 824 and 825. Therefore, the line-printer output should be reformatted to correctly label the mutual impedance phase as an angle.

Figure 2 is a listing of the corrected code for the Linvill coupling method using a z-parameter representation for the two-port model as well as enhanced labeling for the line printer output, as used at the DoD Electromagnetic Compatibility Analysis Center (ECAC).

An example is provided to verify the changes to subroutine OUTPUT. This example consists of a horizontal 0.5 wavelength dipole and a horizontal 0.05 wavelength dipole. Both antennas are situated 0.25 wavelengths above an infinite, perfectly conducting ground plane. The NEC-BSC2.2 input data deck is shown in Figure 3. Figure 4 shows graphs of the outputs from the corrected and uncorrected versions of the NEC-BSC2.2. Also shown, for comparison, are results from the NEC-2 program [Burke and Poggio, 1981] for the same problem. Note that the corrected NEC-BSC2.2 results and the NEC-2 results are in close agreement.

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IF(LWRITE)WRITE(6,250) RXP,TYP,PZP,PRXR,PTYR,PPZR,PRXI,PTYI,PPZI
IF (LPDP) THEN
  IF (LPRR) THEN
    WRITE(22,*)DUMMY, XVARAN, PRXR, PTYR, PPZR
  ELSE
    WRITE(22,*)DUMMY, XVARAN, PRXI, PTYI, PPZI
  END IF
END IF
GO TO 259
258  FQG=FQGS+FQGI*IM
      IF (LWRITE) WRITE(6,251) FQG,PRXR,PTYR,PPZR,PRXI,PTYI,PPZI
      IF (LPDP) THEN
        IF (LPRR) THEN
          WRITE(22,*) DUMMY, FQG, PRXR, PTYR,PPZR
        ELSE
          WRITE(22,*) DUMMY, FQG, PRXI, PTYI,PPZI
        END IF
      END IF
259  IF(I.GT.IMAX) IMAX=IMAX+10*NSN
      IF (LWRITE) THEN
        IF(I.EQ.IMAX) WRITE(6,400)
      END IF
260  CONTINUE
      IF (LWRITE) THEN
        IF(I.NE.IMAX) WRITE(6,400)
        WRITE(6,100)
        WRITE(6,100)
      END IF
      RETURN
800  CONTINUE
C!!!  ANTENNA TO ANTENNA COUPLING REPRESENTATION
      IF (LWRITE) THEN
        WRITE(6,300)
        WRITE(6,100)
        WRITE(6,100)
        WRITE(6,821)
      END IF
821  FORMAT(' ANTENNA COUPLING VIA THE REACTION PRINCIPLE'//)
C
C  INITIALIZE THE COLUMN HEADINGS.
C
      MAGVAL = 'MAGNITUDE'
      PHASEV = 'PHASE'
      MAGG2V = ' GAIN '
      DBVALU = 'GAIN (DB)'
      IF (.NOT. LFQG) THEN
        IF (LRECT) THEN
          VFIRST = 'X'
          VSECND = ' Y '
          VTHIRD = ' Z '
        ELSE
          VFIRST = 'R'
          VSECND = 'THETA'
          VTHIRD = 'PHI'
        END IF
      END IF
      IF (IPRAD .EQ. 1) THEN
        MAGG2V = ' MAG.*2 '
        DBVALU = ' DB '
        WRITE(6,1000)
        WRITE(6,150)
      END IF

```

Figure 2. ECAC's corrected version of the antenna coupling section of NEC-BSC2.2 subroutine OUTPUT.

```

        WRITE(6,2000)
ELSE IF (IPRAD .EQ. 2) THEN
  MAGG2V = 'MAGNITUDE'
  DBVALU = ' PHASE '
  WRITE(6,1010)
  WRITE(6,150)
  WRITE(6,2010)
ELSE IF (IPRAD .EQ. 3) THEN
  WRITE(6,1020)
  WRITE(6,150)
  WRITE(6,2020)
ELSE
  WRITE(6,1030)
  WRITE(6,150)
  WRITE(6,2020)
END IF

C
C   WRITE THE HEADINGS FOR EACH COLUMN.
C
IF (LFQG) THEN
  WRITE(6,2050) MAGVAL, PHASEV, MAGG2V, DBVALU
ELSE
  WRITE(6,2060) VFIRST, VSECOND, VTHIRD, MAGVAL, PHASEV,
  MAGG2V, DBVALU
END IF
END IF
IMAX=10*NSN+1
DO 320 I=NBN,NEN,NSN
IM=I-1
CTM=0.5*BABS(CT(I))
CTP=DPR*BTAN2(AIMAG(CT(I)),REAL(CT(I)))
GO TO (815,830,835,840),IPRAD
UNNORMALIZED REACTION REPRESENTATION
815  CTM2=CTM*CTM
      CTDB=10.*BLOG10(CTM2)
      GO TO 850
C!!!
830  IMPEDANCE REPRESENTATION
Z12=CT(I)/(CI11*CI22)
CTM2=BABS(Z12)
CTDB=DPR*BTAN2(AIMAG(Z12),REAL(Z12))
GO TO 850
C!!!
835  MODIFIED FRIIS' REPRESENTATION
CTM2=0.25*CTM*CTM/(PRAD*PRADR)
CTDB=10.*BLOG10(CTM2)
GO TO 850
C!!!
840  LINVILL REPRESENTATION
Z12=CT(I)/(CI11*CI22)
ZR11 = REAL( Z11 )
ZR22 = REAL( Z22 )
ZZ12=Z12*Z12
ZL=CA8S(ZZ12)/(2.*ZR11*ZR22-REAL(ZZ12))
ZL=ZL*ZL

C
CTM2=0.5*ZL*(1.+0.25*ZZL)
IF(ZL.LT.0.01) GO TO 845
ZZLS=1.-ZZL
CTM2=(1.-SQRT(ZZLS))/ZL
CTDB=10.*BLOG10(CTM2)
CONTINUE
IF(LFQG) GO TO 818
RXP=RXS+RXI*IM
TYP=TYS+TYI*IM
PZP=PZS+PZI*IM
IF ((LPLT) .AND. (.NOT.LFQG)) THEN

```

Figure 2. Continued.

```

        IF(ABS(RXI-TYI).LT.EPSLN) THEN
          IVARAN = 1
        ELSE IF(ABS(TYI-PZI).LT.EPSLN) THEN
          IVARAN = 2
        ELSE
          IVARAN = 3
        END IF
      END IF
      IF (LWRITE) THEN
        WRITE(6,810) RXP,TYP,PZP,CTM,CTP,CTM2,CTDB
      END IF
      IF (LPLT) THEN
        IF (IVARAN .EQ. 1) THEN
          XVARAN = PZP
        ELSE IF (IVARAN .EQ. 2) THEN
          XVARAN = RXP
        ELSE
          XVARAN = TYP
        END IF
        WRITE(19,*)DUMMY,XVARAN,CTDB
      END IF
      GO TO 819
818  FQG=FQGS+FQGI*IM
      IF (LWRITE) THEN
        WRITE(6,811) FQG,CTM,CTP,CTM2,CTDB
      END IF
      IF (LPLT) THEN
        WRITE(19,*) DUMMY,FQG,CTDB
      END IF
819  IF(I.GT.IMAX) IMAX=IMAX+10*NSN
      IF(LWRITE .AND. I.EQ.IMAX) WRITE(6,400)
820  CONTINUE
      IF (LWRITE) THEN
        IF(I.NE.IMAX) WRITE(6,400)
        WRITE(6,100)
        WRITE(6,100)
      END IF
      RETURN
    END

```

Figure 2. Continued.

CM:
 CM:
 CM:
 CE: BSC COUPLING FROM NEC SOURCES
 FR:
 0.3
 US:
 1
 UN:
 1
 LP:
 T
 RG:
 0.,0.,.25
 90.,0.,90.,90.
 -1.,01667,0
 .3551E-3,89.984
 RG:
 -.01667,0.,.25
 90.,0.,90.,90.
 -1.,01667,0
 .1464E-3,89.976
 RG:
 .01667,0.,.25
 90.,0.,90.,90.
 -1.,01667,0
 .1464E-3,89.976
 SG:
 -.22222,0.,.25
 90.,0.,90.,90.
 -1.,05556,0
 .2074E-2,-49.546
 SG:
 -.16667,0.,.25
 90.,0.,90.,90.
 -1.,05556,0
 .4633E-2,-47.518
 SG:
 -.11111,0.,.25
 90.,0.,90.,90.
 -1.,05556,0
 .6282E-2,-44.915
 SG:
 -.05556,0.,.25
 90.,0.,90.,90.
 -1.,05556,0
 .7010E-2,-40.997
 SG:
 .00000,0.,.25
 90.,0.,90.,90.
 -1.,05556,0
 .6863E-2,-35.603
 SG:
 .05556,0.,.25
 90.,0.,90.,90.
 -1.,05556,0
 .7010E-2,-40.997
 SG:
 .11111,0.,.25
 90.,0.,90.,90.
 -1.,05556,0
 .6282E-2,-44.915
 SG:
 .16667,0.,.25
 90.,0.,90.,90.
 -1.,05556,0
 .4633E-2,-47.518
 SG:
 -.22222,0.,.25
 90.,0.,90.,90.
 -1.,05556,0
 .2074E-2,-49.546
 GP:
 0
 PN:
 0.,0.,0.0
 0.,0.,90.,0.
 T
 0.0,0.1,0.25
 0.0,C.1,0.0
 10
 PR:LINVILL
 4
 (0.55803E-2,-0.39955E-2,(0.10204E-6,0.35507E-3)
 (0.11847E+3,0.84823E+2),(0.80936,-0.28163E+4)
 XU:
 EN:

Figure 3. NEC-BSC2.2 input data.

NEC-2/BSC COMPARISON
LINVILL COUPLING METHOD

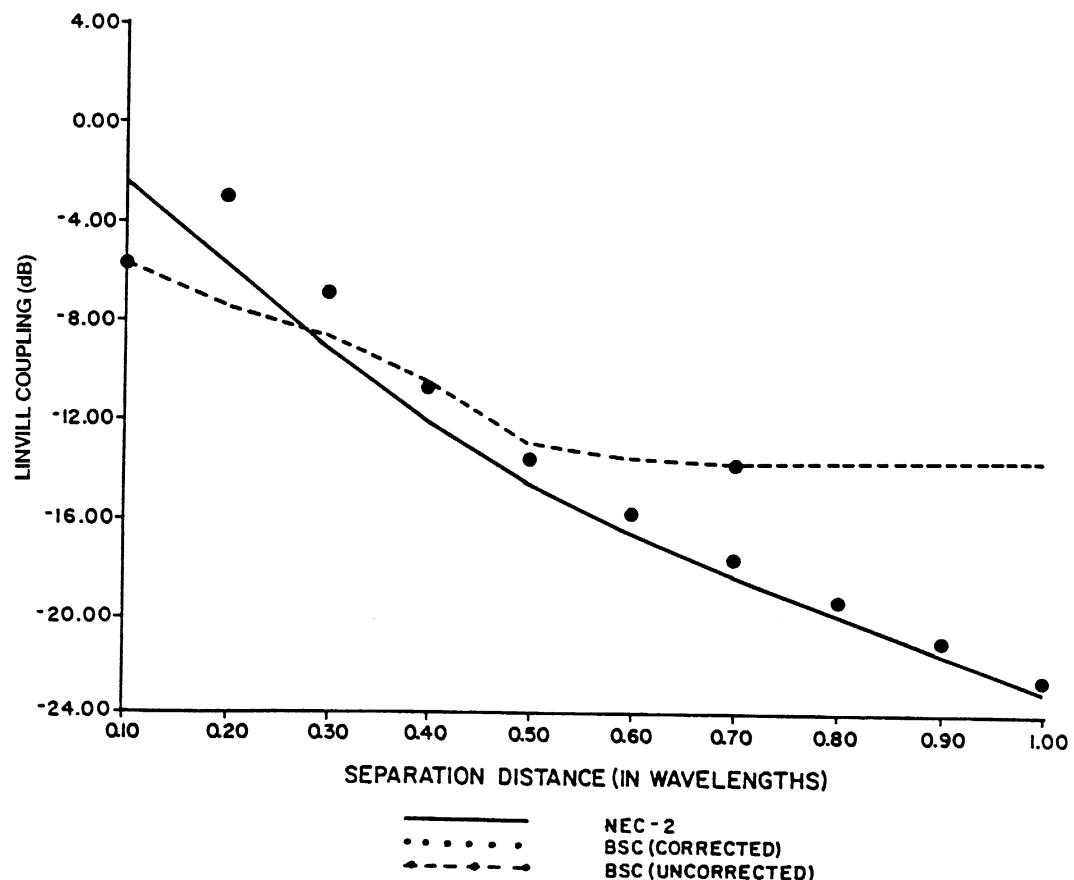


Figure 4. Comparison of corrected and uncorrected BSC coupling outputs with NEC-2 results.

REFERENCES

Burke, G. T., and Poggio, A. T., "Numerical Electromagnetics Code (NEC) - Method of Moments", NOSC TD 116 (3 parts), Naval Ocean Systems Center, San Diego, CA, Revised 1980,81.

Linvill, J. G., and Gibbons, J. F., "Transistors and Active Circuits," McGraw-Hill Book Co., New York, NY, 1961.

Marhefka, R. J., "Numerical Electromagnetic Code-Basic Scattering Code NEC-BSC(Version 2) Part II: Code Manual," The Ohio State University ElectroScience Laboratory, Columbus, OH, December 1982.